## Hertz Contact Mechanics - Verification & Validation

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## Verification and Validation

This section contains a few formulae, which made the listed assumptions, found in the Pre-Analysis & Start-Up page.

The analytical formula for computing the radius of contact zone (a) is given as follows:



The following command for the computation of the contact area can be downloaded here.

• This command was generously provided by Mr. Sean Harvey. (Lead Technical Services Engineer at Ansys Inc.)

	Theoretical	Numerical	Relative Error (%)
Contact radius, a [mm]	1.00964	1.02517	1.538

Using this value of contact radius, we can also compute the normal pressured induced at the contact zone. Theoretically, the maximum pressure ( $p_{max}$ ) is induced along the *y*-axis, as expected, and is given by the following formula:

$$p_{max} = \frac{3F}{2\pi a^2}$$

	Theoretical	Numerical	Relative Error (%)
Max. Pressure, $p_{max}$ [MPa]	88.290	81.094	8.151

Furthermore, we can derive the following formula for the normal stresses  $_{z}$  and  $_{r}$  = along the z-axis.

$$\sigma_{z} = -p_{max} \left( \frac{z^{2}}{a^{2}} + 1 \right)^{-1}$$
$$\sigma_{r} = \sigma_{\theta} = -p_{max} \left[ (1 + \nu_{1}) \left( 1 - \left| \frac{z}{a} \right| \tan^{-1} \left| \frac{a}{z} \right| \right) - \frac{1}{2 \left( \frac{z^{2}}{a^{2}} + 1 \right)} \right]$$

Here we note that the principal normal stresses  $_1 = _2 = _r =$  since the *out-of-plane* shear stresses,  $_{rz} = _z = 0$  and  $_3 = _z$ . And we can deduce that  $_{max} = |_1|=|_2| = |(_1^2)/2|$ . The effective stress (using the *Von-Mises criterion*) along the *y*-axis can be computed as the following:

$$\bar{\sigma} = \frac{1}{\sqrt{2}}\sqrt{(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_1 - \sigma_3)^2}$$

Lastly, we also confirm that the applied load at the top vertex of the sphere matches our numerical contact pressure, integrated along the interface.

Mesh size [m]	2.00E-04	1.00E-04	9.00E-05	Theoretical
Force Reaction (N)	187.95	188.32	188.52	188.50
Relative Error (%)	0.29	0.09	0.01	0.00





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