

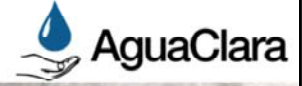
Stacked Rapid Sand (StaRS) Filter Theory

A mathematical model is under development to explain the physics of filtration.

Find more information at [StaRS Filter Theory's wiki](#).

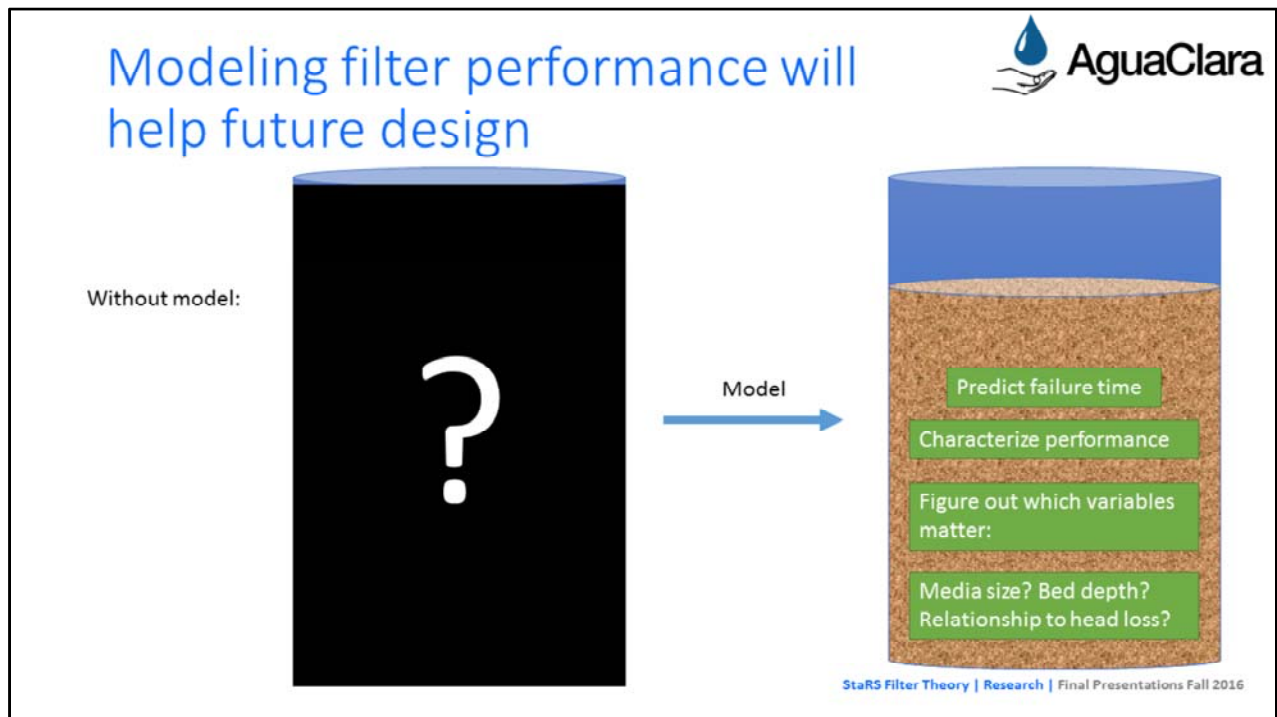


Optimize filter performance for cleaner water



Jonathan
AguaClara plant filter picture
Lab filter picture

The purpose of the StaRS Filter Theory team is understand what is happening in the Stacked Rapid Sand filters
Here is a photo of the AguaClara Filter
Each depth is 20cm, which was arbitrarily chosen
It is not know if this is the optimal depth for a filter



Jonathan

Most models do not explain filtration dynamics, they are called “clean bed” models because they only work when the filter is clean, aka the first few minutes of filter run, after that the models do not work.

Without the models, the filter is just a black box and we do not understand what is happening inside. We hoped with our model to better understand our filter.

Particles collide with sand grains at constrictions



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Jonathan

Sand grains are too small to see, so first we looked at a set of marbles. However, marbles are also pretty small, therefore a set of oranges shown above are used to understand the how a collection of sand grains have extensions and constrictions.

This led to the “constriction model.” We believe that water travels down the filter through a capillary, and that capillary has a number of these constriction. There are a number of capillaries in the filter. As the particles in the water travel down the capillary, as the fluid constrictions, the particles collide and stick to the sand grains.

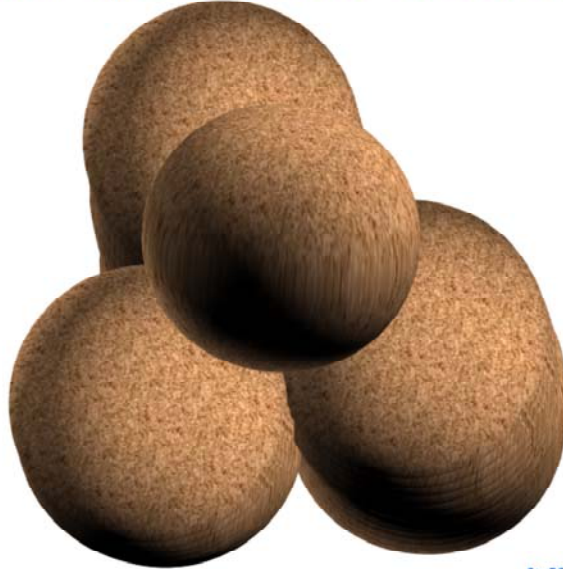
[Particles collide with sand grains](http://www.daviddarling.info/encyclopedia/S/sphere_packing.html)

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Particles build up to create “washers”



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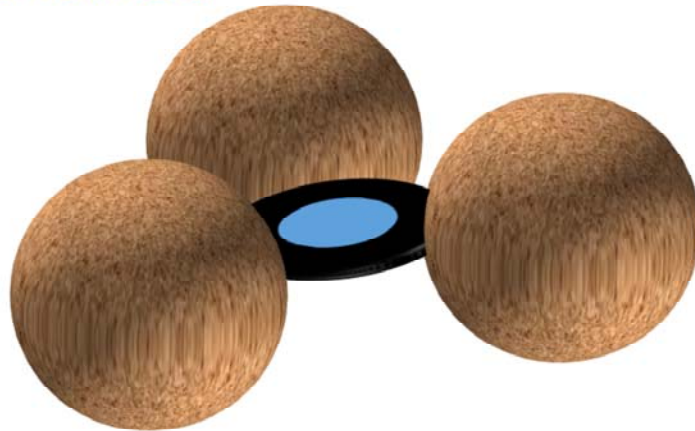
Lucinda

Zoomed in top down, plan view area of the region between sand particles.

Particles attach at the walls of the sand particles forming a washer. As more particles attach and the effective diameter decreases, the washers reach a minimum effective diameter.

This is a result of excessive shear and prevents further particle attachment.

Washers at the constrictions have a small thickness



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If the sand particles were move farther apart, we would be able to see the washer that forms between the three tangent sand particles. In this figure, we can also see that the washers are thin as we expect them to have a very small thickness. In previous assessment of possible models, a very small value was determined for the ratio of captured particle volume to available pore volume. Out of the total available pore volume, only approximately 10^{-3} of the volume is occupied with flocs. The washer model reasonably depicts this as the particles accumulate in thin, small washers.

Streamline
convergence
theory
validates the
washer model

AguaClara

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Lucinda

This diagram is a vertical, cross sectional area of a constriction and expansion. That is if you cut the sand bed down its length. Point out constriction and expansion. Particle capture occurs through the mechanism of interception, where particles collide with the filter media along their paths of travel. **When water flows through the capillary**, streamlines converge at the constrictions increasing interception opportunities. Moreover, **at the site of convergence**, there is a greater number of particles, increasing particle collisions and particle attachment to the constriction wall. **Imagine people running. As the flow continues past the constriction**, the streamlines diverge and particle collisions and attachment to the chamber wall are decreased. **This theory suggests** that there is a very small surface area to which particles can attach to in the filter because **significant accumulation occurs mostly at the constrictions, which have a volume significantly smaller than the expansions**. Therefore, this model **aligns with the calculations** we did in mathcad which demonstrated that the expected volume of accumulated particles is much smaller than total pore volume.

Particles are removed in the active filter zone



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Lucinda

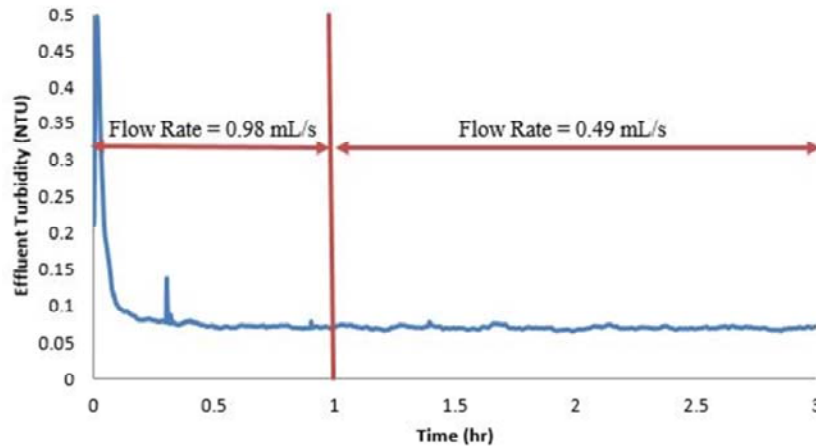
Zoom out of the individual constriction

Look at one capillary tube, for the sake of simplicity, we will only look at a sand filter layer that has top-down flow and we can imagine flocs entering from the top

Three zones we want to look at: dirty bed, clean bed, and active zone. When flocs enter the filter, the active zone starts out at the top of the filter.

Assume active zone is the same length (linear head loss, uniform particle attachment) and dirty and clean bed lengths are changing. Looking at effluent turbidity data, there is slight increase in performance throughout a filtration run and since the only parameters changing during a filtration run is the change in dirty and clean bed lengths, the data suggests that the increase in filter performance is due to the increased length of dirty bed and decreased length in clean bed.

Changing flow rate has no effect on effluent turbidity



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Theresa

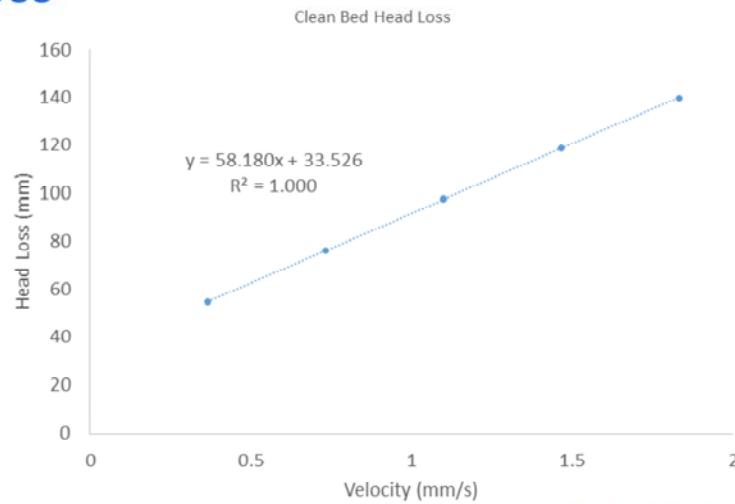
Experiment ran with influent at 5 NTU and 2 mg/L PACl (eventually PID control did not work and influent turbidity changed, but influent turbidity was consistent at 5 NTU for the first 3 hours)

Ran flow rate at full flow rate for 1 hour, then half flow rate

We thought that effluent turbidity would decrease because the lower flow rate meant that there was less shear on the granular media walls (which are also coated with incoming particles), allowing smaller particles to be captured

This hypothesis was not true because effluent turbidity did not change – so particle size doesn't seem to affect the amount that is captured

Only major head loss affects clean bed head loss



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Theresa

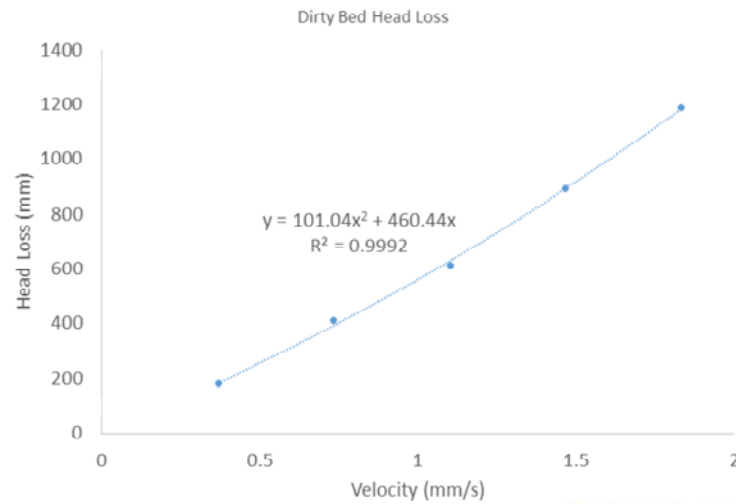
Ran filter at incremental flow rates up to full flow rate (0.98 mL/s)

Head loss is linear with velocity

Follows Carman-Kozeny clean bed head loss which has head loss proportionally linear to velocity

Solved for D_{60} , the effective sand grain size, and got 0.484 mm, which is very close to the sieved estimate of 0.500 mm

Minor losses contribute to dirty bed head loss



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Theresa

Clogged filter at normal flow rate, 5 NTU, 2 mg/L PACl

“Stepped down” flow rate at half the speed and collected head loss readings

Fit the values to a parabolic function, which would follow a head loss based on major losses and minor losses

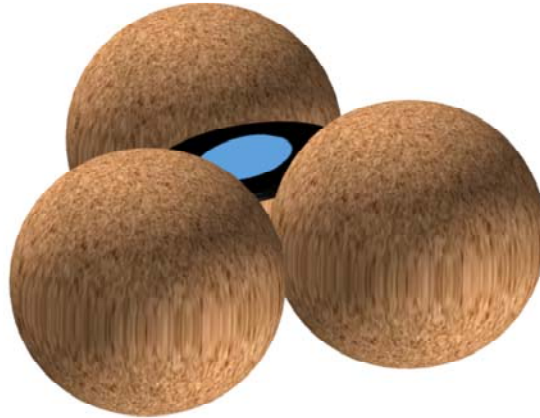
Squared term is minor losses, single term is major losses

Solved for $K = 4579$ with # pores = 400

There are a lot of minor losses

Note change in scale for head loss – there’s a lot more head loss

Washer model is feasible



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Theresa

Minor head loss shows that there are contractions and expansions due to pore restrictions resulting from particles sticking to sand grains and collecting in a washer
These washers of flocs have led to minor losses

Future questions for washer model

How deep is the active layer in the washer model?

What is the height of the washer?

What is the shear force on the washer?

Questions and Recommendations



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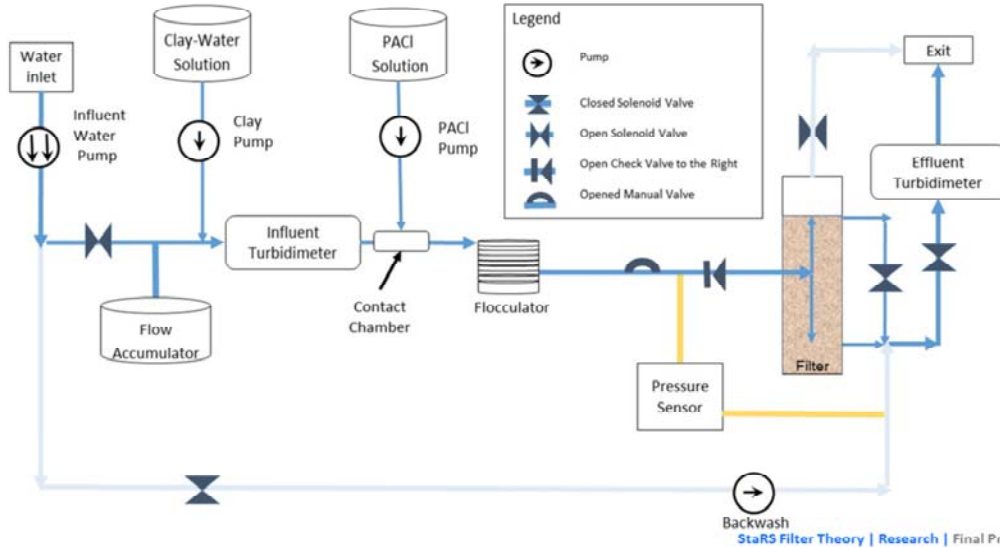
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Appendix Slides



Filter Schematic

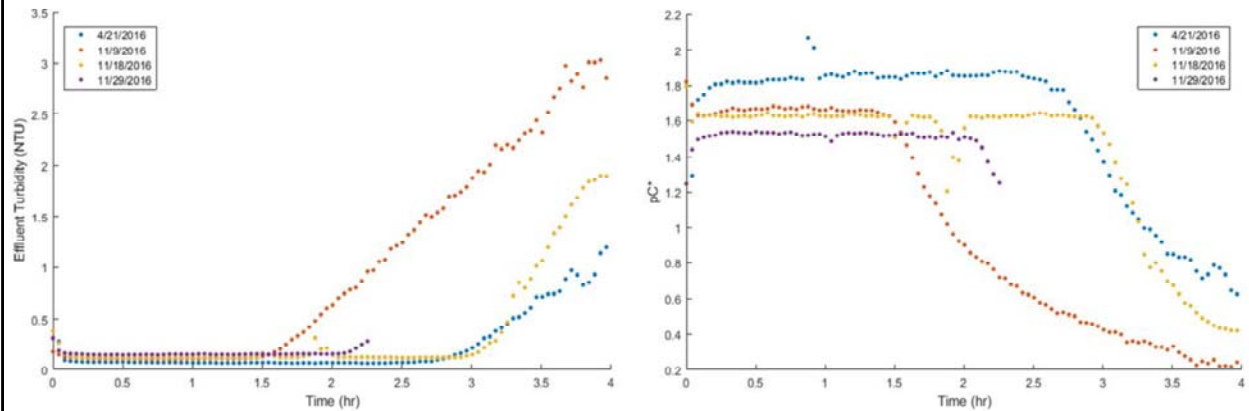


Conditions used to test the filter

- PACl Dosage (mg/L): 0.2, 0.65, 1.1, 1.55, 2
- Influent Turbidity: 5 NTU
 - Variable controlled by PID
- Flow Rate: 118 mL/minute
- Sand Size: Sieved at 30-35
- Procedure
 - Run Time: 12 hours
 - Backwash

Procedure and experimental conditions
PID

Filter performance is inconsistent



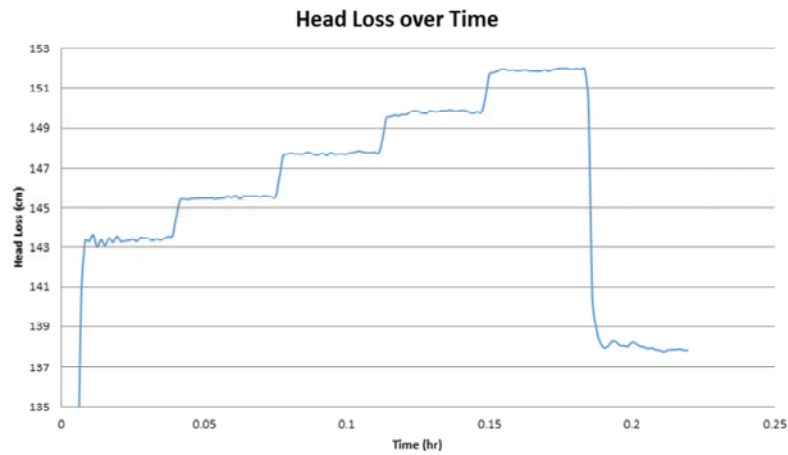
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Theresa

Influent turbidity at 5 NTU, flow rate at 0.98 mL/s, PACl dosage at 2 mg/L – same experiment over and over, but breakthrough/failure times are different for all of them – ranging from 1.5 hours to 3 hours

Two filter runs have similar failure times of 3 hours – but this result is inconsistent with failure times we expected with other coagulant dosages

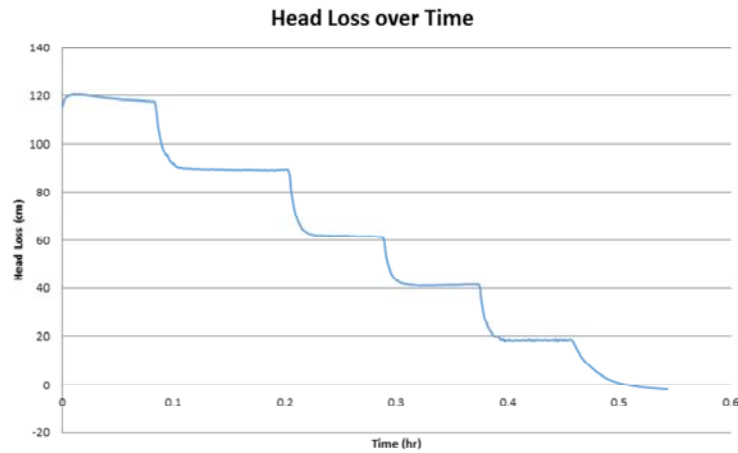
Clean Bed Head Loss



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Clean bed head loss over time during experiment
Each jump up shows an increase in flow rate, thus increasing head loss

Dirty Bed Head Loss



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Dirty bed head loss over time during experiment
Each jump down shows a decrease in flow rate, decreasing head loss